REZULTATI II PARCIJALNOG ISPITA IZ PREDMETA "TEHNIKE PROGRAMIRANJA"

Od ukupno 299 prijavljenih studenata, na ispit je izašlo 285 studenata, od kojih je položilo 118 studenata, što daje prolaznost od oko 41.4 %. Ovo je znatno bolja prolaznost u odnosu na prethodnu akademsku godinu kada je iznosila oko 25.3 %, i godinu prije nje, kada je iznosila oko 30.3 %.. Studentima koji su prethodne akademske godine imali položen drugi parcijalni ispit, a koji su izašli ponovo da pokušaju popraviti broj poena, priznaju se novi bodovi ukoliko su ovaj put položili (čak i ako su eventualno lošiji), a studentima koji nisu ovaj put položili, a imali su od ranije položen I parcijalni ispit, priznaje se 10 poena. Radi boljeg uvida svakog studenta u vlastiti rad, u niže navedenim rezultatima prikazan je ne samo ukupan broj poena koji su studenti postigli na ispitu, nego i broj poena koji su ostvarili na individualnim zadacima.

Indeks	Grupa	Poeni	Z1	Z2	Z3	Z4	Z5	Z6
18376	B	17.4	1.4	3.8	3.0	1.5	2.2	5.5
18403	A	16.4	1.7	1.6	2.6	1.0	6.0	3.5
18116	A	15.9	1.6	1.0	2.0	2.4	5.5	3.4
18504	B	15.9	1.3	3.8	2.8	1.0	2.5	4.5
18094	A	14.4	1.2	1.5	2.3	2.3	3.0	4.1
18356	B	14.1	1.6	3.6	2.5	1.0	0.0	5.4
35−ST	A	13.8	0.9	1.4	2.0	1.5	5.0	3.0
18499	A	13.7	2.0	0.0	2.7	2.2	3.0	3.8
18516	B	13.6	1.3	3.2	2.0	1.0	1.8	4.3
18104	A	13.5	0.0	1.0	2.8	1.0	5.0	3.7
18425	B	13.5	0.3	3.0	2.3	1.5	1.4	5.0
18434	B	13.5	0.6	3.3	2.5	1.6	2.0	3.5
18165	A	13.0	0.8	1.0	2.5	1.5	4.0	3.2
18431	B	13.0	1.0	3.8	1.7	1.5	1.3	3.7
18342	A	13.0	0.9	2.0	2.8	2.3	5.0	0.0
18130	B	12.9	0.0	3.6	0.7	1.6	2.0	5.0
18328	B	12.9	1.2	3.3	2.6	0.1	1.5	4.2
18366	B	12.8	0.9	3.3	1.6	1.5	1.6	3.9
18206	A	12.6	1.8	1.5	0.0	1.5	4.3	3.5
18553	A	12.5	1.5	0.1	2.6	1.6	5.0	1.7
20−ST	B	12.4	0.3	3.2	2.7	1.5	1.2	3.5
18402	A	12.4	1.6	0.0	2.8	0.0	4.5	3.5
18420	A	12.4	1.6	0.8	2.0	1.4	3.3	3.3
18582	B	12.3	1.2	3.6	2.0	0.0	2.0	3.5
18385	A	12.3	1.1	1.2	2.0	1.4	3.3	3.3
18384	A	12.1	1.6	0.0	2.8	1.7	4.0	2.0
31−ST	B	12.0	0.0	3.8	2.7	2.0	0.0	3.5
6−ST	B	12.0	1.8	0.0	2.7	2.0	1.5	4.0
18288	B	12.0	1.3	3.1	2.0	1.0	1.2	3.4
18417	B	12.0	0.0	3.8	0.8	0.7	2.3	4.4
18336	A	12.0	0.6	1.0	2.6	1.3	4.5	2.0
18568	B	11.8	1.3	3.2	2.4	0.3	1.1	3.5
18484	A	11.8	0.5	0.0	2.3	1.2	4.3	3.5
18353	B	11.7	1.7	1.8	2.2	2.0	0.3	3.7
18527	B	11.7	1.3	3.3	2.4	1.5	1.2	2.0
18313	B	11.7	1.5	1.0	2.6	0.0	3.8	2.8
18524	A	11.7	1.0	0.7	2.6	1.4	3.0	3.0
28−ST	B	11.6	0.6	3.5	2.7	0.8	1.0	3.0

18378	A	11.6	0.7	1.0	2.0	2.3	3.8	1.8
18235	A	11.6	0.0	1.5	2.5	1.4	4.4	1.8
18292	A	11.6	0.3	1.5	0.0	1.5	5.0	3.3
18151	B	11.5	1.7	3.4	0.6	1.0	1.5	3.3
18509	A	11.4	0.0	3.7	2.4	0.8	0.0	4.5
18374	A	11.4	0.0	1.2	1.8	1.3	3.8	3.3
18511	A	11.4	0.6	0.8	2.7	0.5	3.3	3.5
18285	B	11.3	0.7	3.5	2.5	0.3	1.0	3.3
18555	A	11.3	1.0	0.1	2.4	1.3	3.3	3.2
18367	B	11.2	0.0	3.0	2.4	1.2	1.5	3.1
18444	B	11.2	0.3	3.0	2.4	0.8	1.5	3.2
18361	B	11.2	0.0	0.1	2.8	1.0	4.0	3.3
18519	B	11.0	0.4	1.0	2.2	1.8	2.5	3.3
18383	B	11.1	1.1	3.4	2.3	0.2	0.0	4.1
18163	B	11.1	0.0	3.2	2.0	1.0	1.4	3.5
18213	A	11.1	0.1	0.0	2.5	1.5	3.7	3.3
18338	A	11.0	1.6	1.0	2.7	1.3	2.8	1.6
18323	A	11.0	1.3	0.6	0.5	1.2	3.8	3.6
18365	A	11.0	1.8	0.1	2.5	0.1	4.0	2.5
18230	B	10.9	0.0	3.0	2.0	0.0	1.7	4.2
18480	B	10.9	0.3	3.2	2.2	0.0	1.4	3.8
18495	B	10.9	0.9	1.0	0.6	1.6	3.8	3.0
17845	B	10.8	1.7	3.0	0.0	0.8	1.5	3.8
18112	B	10.7	0.9	3.3	1.8	0.7	1.0	3.0
18115	A	10.7	0.7	1.5	1.8	0.0	4.0	2.7
18463	A	10.7	0.0	0.7	0.0	2.3	5.7	2.0
18343	A	10.7	1.6	0.8	2.7	2.3	0.1	3.2
18255	A	10.6	0.9	0.7	0.4	1.4	4.3	2.9
18536	B	10.6	1.3	3.7	2.6	1.0	0.0	2.0
18310	B	10.5	0.4	3.5	2.0	0.2	1.4	3.0
18389	B	10.5	1.2	3.8	0.0	0.1	1.4	4.0
18547	B	10.5	0.7	3.8	1.8	1.2	0.0	3.0
17867	B	10.5	0.0	2.4	2.6	1.0	1.6	2.9
18324	B	10.5	0.7	3.4	2.6	0.0	0.0	3.8
18355	A	10.5	0.0	0.0	2.8	0.0	5.3	2.4
18529	A	10.5	0.0	0.0	2.0	1.5	3.8	3.2
18105	B	10.4	1.3	3.2	0.0	1.5	1.7	2.7
18371	A	10.4	0.0	1.0	2.4	0.7	3.3	3.0
18416	A	10.4	0.6	0.5	1.5	1.5	3.0	3.3
18537	A	10.4	0.0	0.5	2.0	1.0	3.5	3.4
18305	B	10.3	1.0	3.3	0.0	1.5	2.2	2.3
17862	A	10.3	0.0	1.5	2.3	0.0	3.0	3.5
18479	A	10.3	1.6	0.0	2.7	1.5	4.5	0.0
18565	A	10.2	1.0	0.7	2.0	1.0	2.7	2.8
18413	B	10.2	0.6	3.2	1.3	1.0	0.7	3.4
18352	A	10.2	1.6	1.0	2.6	1.0	1.5	2.5
18251	B	10.2	2.0	3.4	0.0	0.0	1.5	3.3
18301	A	10.2	1.6	0.1	2.5	0.2	3.3	2.5
18076	B	10.0	1.0	3.2	0.2	1.2	1.0	3.4
18177	A	10.0	0.0	0.0	2.2	1.0	3.8	3.0
18326	B	10.0	0.8	0.0	2.8	1.5	1.1	3.8
18195	B	10.0	1.6	3.0	2.0	0.5	0.5	2.4
18085	B	10.0	0.0	2.8	2.5	0.2	1.5	3.0
16603	A	10.0	0.6	1.5	0.0	1.5	3.1	3.3

18222	A	10.0	0.4	2.0	0.0	2.3	1.3	4.0
18347	B	10.0	0.8	3.3	2.5	0.0	0.0	3.4
18447	A	10.0	0.8	1.5	2.2	0.0	2.3	3.2
18496	B	10.0	0.9	3.0	2.2	0.1	0.3	3.5
18350	B	10.0	0.9	3.0	2.7	0.1	0.0	3.3
18240	A	10.0	0.4	1.0	2.7	1.2	4.7	0.0
18238	B	10.0	0.0	0.5	2.7	0.0	4.1	2.7
18208	A	10.0	0.0	1.5	0.0	1.2	3.5	3.8
18315	A	10.0	1.6	0.0	0.0	1.5	5.1	1.8
18445	A	10.0	0.0	1.0	2.5	1.2	3.8	1.5
18257	A	10.0	0.9	0.0	0.0	1.0	4.6	3.5
18483	A	10.0	0.3	1.5	2.6	0.1	5.5	0.0
18148	A	10.0	0.0	0.3	2.6	1.6	2.8	2.7
18198	A	10.0	0.9	0.0	2.6	0.4	3.1	3.0
17801	B	10.0	0.4	3.3	0.0	0.7	1.5	4.1
18044	A	10.0	0.0	0.8	2.0	1.2	2.7	3.3
18364	B	10.0	0.0	3.4	2.0	1.0	0.8	2.8
18348	A	10.0	0.0	0.0	2.8	0.0	3.8	3.4
18393	B	10.0	0.0	3.8	2.6	0.0	0.0	3.6
18423	A	10.0	0.9	0.8	1.5	1.3	2.7	2.8
18246	B	10.0	1.5	3.0	0.0	1.0	2.0	2.5
18036	A	10.0	0.9	0.5	2.0	0.7	3.5	2.4
18572	A	10.0	0.3	0.2	2.8	1.0	3.3	2.4
18307	B	10.0	1.2	3.5	0.1	0.0	2.0	3.2
18435	A	10.0	1.0	0.2	1.5	1.2	2.7	3.4
18507	A	10.0	0.9	0.8	2.5	1.1	3.1	1.6
19−ST	A	9.0	1.0	0.4	0.2	1.4	3.3	2.7
18126	B	9.0	0.9	3.3	0.0	1.0	1.3	2.5
18589	B	9.0	1.4	3.4	1.3	0.8	1.5	0.6
18330	B	9.0	1.2	3.2	0.0	1.5	0.7	2.4
18160	B	9.0	1.3	3.0	0.0	1.0	0.0	3.7
18129	A	9.0	0.9	0.8	0.0	1.5	2.5	3.3
18375	B	9.0	0.0	3.0	1.5	0.1	2.0	2.4
18304	B	9.0	1.4	3.0	0.0	0.0	1.2	3.4
18357	B	9.0	1.2	3.8	0.0	0.5	0.0	3.5
18477	B	9.0	0.0	3.5	2.0	1.0	0.5	2.0
18098	B	8.9	0.0	3.4	1.8	1.0	1.2	1.5
18079	A	8.9	0.9	0.0	0.0	1.5	3.5	3.0
18150	A	8.9	0.3	1.5	0.0	1.2	2.6	3.3
18392	B	8.8	0.0	3.2	0.0	0.8	1.5	3.3
18508	A	8.8	0.0	1.0	2.3	0.0	4.0	1.5
18209	A	8.8	0.6	0.0	0.0	2.0	3.2	3.0
18118	A	8.8	0.9	1.2	0.0	0.5	3.0	3.2
17815	B	8.7	0.9	3.3	0.0	0.0	1.7	2.8
18523	B	8.7	0.0	3.4	0.0	1.0	0.3	4.0
17268	A	8.7	0.9	0.5	1.6	0.0	3.3	2.4
18203	A	8.7	1.8	0.0	0.7	0.0	3.5	2.7
18556	B	8.6	0.0	2.6	1.5	0.0	1.2	3.3
18472	A	8.5	0.7	1.5	0.5	1.5	1.0	3.3
18489	A	8.5	1.3	0.2	2.0	0.0	2.0	3.0
18245	A	8.5	0.0	0.0	0.0	1.0	4.0	3.5
17309	B	8.5	1.3	3.0	1.8	0.1	0.0	2.3
18187	A	8.5	0.0	0.2	0.0	1.0	4.0	3.3

18030	B	8.4	1.0	3.2	0.7	0.7	1.3	1.5
18481	A	8.3	1.1	0.2	0.1	0.4	3.5	3.0
18493	B	8.2	0.6	3.6	0.0	0.5	0.0	3.5
18239	B	8.1	1.7	2.8	0.0	1.0	0.0	2.6
17047	A	8.1	1.2	1.0	0.0	1.6	1.5	2.8
17948	A	8.1	0.4	0.0	2.0	0.0	2.3	3.4
18538	B	8.1	0.0	3.3	0.0	0.0	0.0	4.8
18584	A	8.1	0.6	1.0	0.0	0.0	3.5	3.0
18318	B	8.0	0.9	3.5	0.0	0.8	0.0	2.8
18054	A	8.0	1.3	0.1	0.0	0.8	2.8	3.0
18181	B	8.0	0.8	3.0	0.0	0.9	0.9	2.4
17906	B	8.0	0.0	3.4	0.0	0.9	1.2	2.5
18136	A	8.0	0.0	0.1	1.5	0.4	3.0	3.0
17932	B	8.0	0.0	1.8	0.0	0.0	1.0	5.2
18460	B	8.0	0.0	3.3	0.2	0.5	0.0	4.0
18457	B	7.9	0.9	3.4	0.0	0.0	0.0	3.6
18400	B	7.9	0.9	3.0	1.3	0.1	1.3	1.3
18172	B	7.9	0.0	3.4	0.0	0.5	1.0	3.0
18139	B	7.8	0.1	2.8	0.0	0.0	1.4	3.5
18225	A	7.8	1.2	0.4	0.0	1.0	4.0	1.2
18456	B	7.7	1.7	3.0	0.2	1.2	0.8	0.8
17639	B	7.7	0.0	2.8	1.5	0.1	0.3	3.0
32−ST	A	7.6	1.0	0.0	0.0	2.0	1.3	3.3
17991	A	7.6	0.9	0.5	0.7	0.7	1.5	3.3
18359	B	7.6	0.9	2.9	1.3	0.0	0.0	2.5
18430	B	7.5	0.9	3.1	0.0	0.0	1.0	2.5
18514	B	7.5	1.0	3.3	2.4	0.1	0.7	0.0
18224	A	7.4	1.3	0.0	0.0	0.0	2.7	3.4
18108	A	7.3	0.9	1.2	0.0	1.3	2.5	1.4
18344	A	7.3	0.0	0.5	1.7	1.5	0.0	3.6
18485	A	7.3	0.9	0.8	0.0	1.6	0.7	3.3
18314	A	7.3	0.9	0.8	0.0	0.0	3.6	2.0
22−ST	A	7.2	0.9	0.8	2.4	0.8	2.3	0.0
18202	B	7.2	0.3	3.4	0.0	1.0	0.0	2.5
18533	A	7.2	1.6	0.1	0.3	0.7	1.5	3.0
17809	A	7.1	0.5	0.0	0.0	1.2	2.7	2.7
18196	B	7.1	0.0	3.2	0.0	0.3	0.3	3.3
17844	B	7.1	1.0	3.0	0.0	0.2	0.0	2.9
18540	B	7.1	2.0	1.4	0.0	0.0	0.0	3.7
18418	B	7.0	0.0	3.4	0.0	0.8	0.5	2.3
18135	B	6.9	0.0	3.3	0.0	0.0	0.8	2.8
18441	B	6.9	1.0	3.3	0.0	0.8	1.0	0.8
18204	A	6.9	1.2	0.3	0.0	0.0	2.6	2.8
18570	A	6.9	0.7	0.3	1.0	0.7	1.2	3.0
18510	B	6.8	0.0	2.8	0.0	1.0	1.5	1.5
17984	A	6.8	1.2	1.3	0.6	1.2	0.0	2.5
17966	B	6.8	1.0	2.9	0.0	0.1	1.0	1.8
18422	A	6.8	1.0	0.5	0.0	1.3	1.0	3.0
18012	A	6.7	0.0	0.5	0.0	0.5	2.7	3.0
18221	B	6.6	0.0	3.2	0.0	1.0	0.8	1.6
18541	B	6.5	0.0	3.8	2.7	0.0	0.0	0.0
18358	A	6.4	0.9	0.0	0.0	1.3	2.7	1.5
18490	A	6.4	0.9	0.3	0.0	1.5	3.7	0.0
17731	A	6.3	0.7	1.5	0.0	1.3	2.8	0.0

26−ST	A	6.2	0.8	0.5	0.0	0.0	2.5	2.4
18244	B	6.2	1.2	3.5	0.0	0.1	0.1	1.3
18254	A	6.2	1.3	0.8	0.0	0.5	1.6	2.6
18544	B	6.0	0.3	2.7	0.0	0.0	0.0	3.0
17982	A	6.0	0.0	0.3	1.0	1.0	1.2	2.5
18133	A	6.0	0.0	0.1	0.6	0.0	3.0	2.3
17520	B	5.9	0.7	3.0	0.0	0.4	1.0	0.8
36−ST	B	5.8	0.4	3.0	0.0	0.0	0.0	2.4
18363	B	5.8	0.9	2.7	1.5	0.0	0.0	0.7
18583	A	5.7	0.2	1.0	0.0	0.3	1.0	3.2
18379	B	5.7	1.2	2.8	1.3	0.1	0.0	0.3
18453	B	5.6	0.0	3.0	0.0	0.0	0.8	1.8
17627	A	5.6	0.9	0.1	0.0	1.4	1.5	1.7
18311	B	5.3	1.0	2.6	0.0	0.5	0.0	1.2
18286	B	5.3	1.2	3.2	0.0	0.2	0.4	0.3
18269	B	5.2	0.0	2.7	0.0	0.0	0.0	2.5
18433	B	5.2	0.0	3.4	0.0	0.1	0.0	1.7
17642	B	5.2	0.0	2.6	0.0	1.0	0.0	1.6
18072	A	5.2	0.3	0.5	0.6	1.2	2.6	0.0
18578	B	5.1	1.2	3.2	0.0	0.0	0.0	0.7
18443	A	5.1	0.6	0.3	0.2	0.6	2.8	0.6
18170	B	5.0	0.6	3.0	0.1	0.1	0.0	1.2
18042	A	5.0	0.0	0.5	0.0	1.0	0.3	3.2
17750	B	5.0	0.8	2.7	0.0	0.1	0.0	1.4
18395	A	5.0	1.2	0.0	0.0	0.0	1.0	2.8
18377	B	5.0	0.3	3.5	0.0	0.5	0.6	0.1
18295	A	4.8	1.4	0.2	0.0	0.0	0.5	2.7
17234	A	4.7	0.9	0.0	0.0	0.0	1.5	2.3
18459	B	4.7	1.7	3.0	0.0	0.0	0.0	0.0
18199	A	4.7	1.2	0.1	0.0	0.0	0.8	2.6
18349	B	4.6	1.0	3.3	0.0	0.3	0.0	0.0
17820	B	4.5	0.0	3.0	0.0	0.5	0.0	1.0
18593	A	4.5	1.3	0.1	0.0	0.0	1.1	2.0
18391	A	4.4	0.6	0.2	0.2	0.0	0.4	3.0
17949	B	4.3	0.9	2.8	0.0	0.1	0.5	0.0
17898	A	4.3	0.0	0.0	0.0	0.0	1.3	3.0
25−ST	B	4.3	1.0	2.3	0.0	0.1	0.0	0.9
18462	A	4.3	0.0	2.8	0.0	0.0	0.0	1.5
24−ST	B	4.2	0.9	0.3	0.0	0.0	0.8	2.2
18102	A	4.2	0.0	0.2	0.0	0.5	0.5	3.0
18237	B	4.1	0.9	2.3	0.0	0.0	0.7	0.2
18410	A	4.1	0.9	0.0	0.0	0.0	0.0	3.2
17972	B	3.9	0.0	1.4	0.0	0.5	0.0	2.0
17899	B	3.9	0.0	3.2	0.0	0.1	0.0	0.6
17629	A	3.9	1.0	0.1	0.0	0.0	0.8	2.0
18081	B	3.9	0.9	3.0	0.0	0.0	0.0	0.0
18390	A	3.9	0.3	0.0	0.0	0.6	0.0	3.0
47−ST	B	3.8	0.0	1.5	0.0	0.0	0.0	2.3
18280	A	3.8	1.2	0.3	0.0	0.0	0.6	1.7
18316	A	3.8	0.3	0.1	0.0	0.6	0.1	2.7
18189	B	3.7	0.0	3.3	0.2	0.1	0.0	0.1
18073	A	3.7	0.5	0.0	0.0	1.0	2.2	0.0
17487	B	3.3	0.0	2.7	0.0	0.0	0.0	0.6
17348	B	3.3	0.0	3.3	0.0	0.0	0.0	0.0

13−ST	A	3.2	0.8	0.0	0.1	0.0	0.0	2.3
17200	B	3.1	0.0	0.3	0.0	1.0	0.0	1.8
18087	B	3.1	0.6	1.7	0.0	0.1	0.0	0.7
18464	B	3.1	0.0	2.5	0.0	0.0	0.0	0.6
18210	B	3.0	0.5	2.5	0.0	0.0	0.0	0.0
18075	A	3.0	0.2	0.3	0.0	0.0	0.5	2.0
16802	B	2.8	0.1	2.7	0.0	0.0	0.0	0.0
18060	B	2.8	1.2	1.4	0.1	0.1	0.0	0.0
18128	A	2.7	1.0	0.2	0.0	0.0	0.5	1.0
17166	A	2.7	0.0	0.0	0.0	0.0	0.0	2.7
17422	A	2.7	1.0	0.0	0.0	0.0	0.2	1.5
18188	A	2.6	0.9	0.2	0.0	0.0	0.0	1.5
17081	A	2.6	0.0	0.1	0.0	1.3	1.2	0.0
18066	B	2.4	0.0	2.4	0.0	0.0	0.1	0.0
17189	A	2.4	0.0	0.0	0.0	0.0	0.0	2.4
18534	B	2.4	0.2	2.0	0.1	0.0	0.0	0.1
16429	B	1.9	0.9	0.6	0.3	0.1	0.0	0.0
18256	B	1.9	0.3	0.7	0.1	0.1	0.0	0.7
18396	A	1.6	1.3	0.1	0.1	0.0	0.0	0.1
17734	A	1.6	1.2	0.2	0.2	0.0	0.0	0.0
17742	A	1.6	1.0	0.1	0.0	0.0	0.0	0.5
18331	A	1.6	0.0	0.4	0.0	0.7	0.0	0.5
18218	A	1.5	0.0	0.5	0.0	0.0	0.0	1.0
18093	B	1.4	0.6	0.8	0.0	0.2	0.0	0.0
18401	A	1.4	0.1	0.2	0.7	0.0	0.1	0.3
18161	B	1.3	0.0	1.3	0.0	0.0	0.0	0.0
37−ST	B	0.7	0.0	0.7	0.0	0.0	0.0	0.0
17653	B	0.6	0.0	0.2	0.0	0.0	0.1	0.3
18517	B	0.4	0.0	0.4	0.0	0.0	0.0	0.0
16−ST	A	0.1	0.1	0.0	0.0	0.0	0.0	0.0
18171	B	0.1	0.0	0.1	0.0	0.0	0.0	0.0
14−ST	B	0.0	0.0	0.0	0.0	0.0	0.0	0.0

U ponedjeljak, 1. VII 2019. godine u 15.30 u velikom amfiteatru održaće se javna prezentacija rješenja uz diskusiju, nakon koje slijedi uvid u radove za one studente kojima ni nakon održane prezentacije još uvijek nije jasno šta nisu uradili kako treba (prezentaciji mogu prisustvovati i studenti koji ne žele ostati na uvidu).

O terminu završnog ispita studenti će biti obaviješteni putem Zamgera.

Predmetni nastavnik:

Red. prof. dr. Željko Jurić